## WOODLAND ENVIRONMENTAL

## CHERRY LODGE GOLF CLUB, BIGGIN HILL

REVISED CONSTRUCTION TRAFFIC MANAGEMENT STATEMENT


REPORT REF. F990-02A

## CHERRY LODGE GOLF CLUB, BIGGIN HILL

## REVISED CONSTRUCTION TRAFFIC MANAGEMENT STATEMENT

## CONTENTS

Page
1.0 INTRODUCTION ..... 1
2.0 EXISTING SITUATION ..... 2
3.0 CONSTRUCTION TRAFFIC MANAGEMENT ..... 4
4.0 SUMMARY AND CONCLUSIONS ..... 14
DRAWINGS
F990-003A PROPOSED TEMPORARY ACCESS
APPENDICES
APPENDIX A WOODLAND ENVIRONMENTAL HAUL ROAD ROUTESDRAWINGS
APPENDIX B PUBLIC RIGHTS OF WAY MAP
APPENDIX C TRAFFIC SPEED SURVEY RESULTSAPPENDIX D STAGE 1 ROAD SAFETY AUDIT
APPENDIX E RESULTS OF TRAFFIC SURVEY ON MAIN ROAD ANDPICADY CAPACITY ASSESSMENT OF PROPOSEDJUNCTION WITH HAUL ROAD

## DOCUMENT CONTROL SHEET

| REV | ISSUE PURPOSE | AUTHOR | CHECKED | APPROVED | DATE |
| :---: | :--- | :---: | :---: | :---: | :---: |
| - | $1^{\text {st }}$ Draft Client Issue | SAF | CMB | DJR | $11 / 03 / 11$ |
| - | Final | SAF | CMB | DJR | $14 / 07 / 11$ |
| A | Revised draft to address <br> LBB concerns | ML | SAF | ML | $11 / 10 / 11$ |
| A | Final Revision | ML | SAF | ML | $18 / 10 / 11$ |
| A | Final Revision with <br> amendments for <br> submission | ML | SAF | ML | $20 / 10 / 11$ |

### 1.0 INTRODUCTION

1.1 Ardent Consulting Engineers (ACE) has been appointed by Woodland Environmental (WE) to advise on construction traffic management for the upgrading and modernisation of the Cherry Lodge Golf Club, Biggin Hill.
1.2 A Construction Traffic Management Statement (CTMS) was prepared in support of the planning application (ref 11/02499) for submission to the local planning and highway authority, the London Borough of Bromley (LBB) in July 2011. This Revised CTMS has been prepared to address concerns raised by LBB on highways grounds in their response dated $30^{\text {th }}$ August 2011.
1.3 The planning application is also supported by a Transport Statement, also prepared by ACE, which has also been revised to address comments made by LBB.
1.4 Following this introduction, the remainder of this report is structured as follows:

- Section $\mathbf{2 . 0}$ describes the existing situation;
- Section $\mathbf{3 . 0}$ outlines the proposed management of construction traffic and;
- Section 4.0 provides a summary and sets out the conclusions.


### 2.0 EXISTING SITUATION

## Site Location

2.1 The site which forms the subject of this planning application is located on the eastern fringe of Biggin Hill, as shown at Plate 1.


Plate 1: Site Location

## Site Access

2.2 The site is accessed from Jail Lane, which runs on an east-west alignment to the immediate north of the site. Jail Lane varies in character along its length, it being a circa 7 m wide urban single carriageway road with footways as it passes through residential development immediately east of the A233, and narrowing to a circa 4.3 m wide semi-rural lane beyond this. The site access is taken from the semi-rural lane section, the width of which allows two cars to pass only.

## Local Highway Network

2.3 The A223 Main Road is a circa 7.3 m wide single carriageway road that is subject to a 30 mph speed limit. It also has a local weight restriction, with access restricted to sub 5-tonne vehicles only in the hours 6:30pm - 8:00am. In addition, LBB is part of the Transport for London (TfL) Low Emission Zone (LEZ).

## Strategic Highway Network

2.4 The A223 connects to the A232 at Bromley Common to the north and the A25 at Westerham to the south, both via priority ' T ' junctions. The A25 connects to Junction 5 of the M25 near Sundridge. The M26 and A21 also connect with the M25 at this junction. There is no exit from the M26 to the M25 and all traffic must join the clockwise (westbound) M25. Plate 2 illustrates the strategic highway network in the wider local area.


Plate 2: Strategic Highway Network

### 3.0 CONSTRUCTION TRAFFIC MANAGEMENT

## Site Access

3.1 Jail Lane is considered unsuitable for frequent HGV use given that its narrow width in the vicinity of the existing Golf Club access does not allow for a HGV to pass a car. Therefore, it is not intended to use the existing site access for construction access.
3.2 It is proposed to provide temporary construction access to the site from the A223 Main Road in proximity to an existing farm access on Main Road (see Plate 3). WE has agreed a haul road route that borders agricultural land with the landowner; this has been revised since the original scheme proposals, as shown in WE drawing nos 100.23 rev C and 100.24 Rev C, attached at Appendix A.
3.3 The revised proposals now include a compound inside the site, thought the wheel washing facility has been provided close to the site entrance and on the haul road itself to avoid unnecessary crossings of the Byway. A small ticketing office ( $6 \mathrm{~m} \times 3 \mathrm{~m}$ ) is located next to the wheel washing facility to supervise access and ticket vehicles upon entry.
3.4 The haul road would be at least 6 m wide along its initial section to allow for two-way HGV movements and would route alongside and segregated from an existing byway, with a $10-15 \mathrm{~m}$ wide buffer between the two.


Plate 3: Site Access Location
3.5 The temporary haul road is proposed to connect to Main Road via a new priority ' $T$ ' junction arrangement. Proposed radii between Main Road and the haul road are 10 m to ensure that vehicles turning leftin or out do not conflict with traffic travelling northbound on Main Road, and this is demonstrated in the swept path assessment shown on Drawing no. F990-003A.
3.6 The proposed temporary junction arrangement is located close to the points at which Byway BR283 and Bridleway BR275B (upgraded from Footpath status in 2010) meet and connect to Main Road (see map enclosed at Appendix B). The junction design includes footways around its radii to provide alternative connections to these Public Rights of Way (PRoW) for walkers, whilst the Byway/Bridleway connection to Main Road is retained as a vehicular crossover. Banksmen will be deployed during site operating hours to ensure the safety of walkers crossing the haul road.
3.7 A gate will be provided across the haul road behind the point where Byway BR283 crosses, and this will be closed outside of site operating hours to prevent unauthorised access.
3.8 Main Road is subject to a 30 mph speed limit in the vicinity of the proposed access. In pre-application discussions, LBB requested that a speed survey be undertaken to verify $85^{\text {th }}$ percentile traffic speeds to inform junction visibility splay requirements.
3.9 A traffic speed survey on a sample of 100 vehicles in each direction was undertaken at Main Road in dry weather on two days in June 2009 in accordance with guidance set out in TA 22/81 Vehicle Speed Measurement on All Purpose Roads. This showed $85^{\text {th }}$ percentile northbound and southbound dry weather speeds of 37 mph ( 60 kph ) and 39 mph ( 63 kph ) respectively. The speed survey results are included at Appendix C.
3.10 The required ' $y$ ' distances for visibility splays at junctions on an existing road are based on the stopping site distance (SSD) of vehicles travelling on the major road at the observed $85^{\text {th }}$ percentile speed in wet weather conditions. Subtracting 4 kph from the dry weather speeds (as stipulated in TA 22/81) gives $85^{\text {th }}$ percentile wet weather speeds of 35 mph ( 56 kph ) northbound and 37 mph ( 59 kph ) southbound.
3.11 In pre-application discussions with LBB, it was established that the use of the parameters recommended in the Manual for Streets (MfS) may be acceptable to derive the SSD on Main Road. In this respect, MfS states that its guidance on SSDs applies where $85^{\text {th }}$ percentile speeds do not exceed 37 mph ( 60 kph ), as is the case at Main Road.
3.12 The visibility requirements in the MfS are based on a driver perception/reaction time of 1.5 seconds, and a deceleration rate of 0.45 g . Applying these constants to the $85^{\text {th }}$ percentile wet weather
speeds gives SSDs (adjusted for bonnet length) of 53 m for northbound vehicles and 57 m for southbound vehicles.
3.13 Given the nature of the use of the temporary construction access, and as agreed with LBB, an ' $x$ ' distance of 2.4 m is considered appropriate. Pending the cutting back of hedgerow, visibility splays of $2.4 \mathrm{~m} \times 53 \mathrm{~m}$ and 57 m are achievable looking left (south) and right (north), respectively, along Main Road for drivers egressing the site, as shown on Drawing no. F990-003B. It is relevant to note that the hedgerow located within the visibility splay to the right is already maintained at a low level to allow for greater visibility for vehicles egressing the Byway.
3.14 In terms of visibility in the vertical plane, TD 9/93 Highway Link Design identifies that SSD should be measured from a driver's eye height of between 1.05 m and 2.00 m , to an object height of between 0.26 m and 2.00 m above the road surface. These eye height dimensions are relevant to a car driver and HGV driver respectively. Given that the access will be used exclusively by HGVs, it was originally anticipated that the hedgerow would be cut back to allow visibility from a 2.00 m driver eye height. However, following comments raised in the Safety Audit requested by LBB, which is attached at Appendix D, sufficient visibility will be provided in each direction along Main Road from a car driver's eye height of 1.05 m , requiring the hedge height to be reduced further. This also addresses a request made by LBB that visibility splays be provided for this eye height.
3.15 As requested by LBB, despite the very low volume of traffic turning into and out of the haul road at the proposed access, a capacity assessment has been undertaken using the industry-standard software PICADY. The analysis is based on the maximum two-way hourly flow observed on Main Road during the inter-peak period (between 09:00 and 17:00) on a weekday on Tuesday 27th

September 2011 (during school term time). This was 915 vehicles and occurred between 16:00-17:00 (i.e. partly outside the hours of site operation so use of the flows in this period is an onerous assumption). The survey results are attached at Appendix $\mathbf{E}$.
3.16 To be robust we have assumed 15 HGVs arriving at the site from the south and turning right into the haul road in an hour, with 15 HGVs departing the site and turning right onto Main Road during this hour. This compares with the average of 10 arrivals and 10 departures per hour expected during each weekday throughout the construction period (see below). We have also used the ODTab facility to model a 90 -minute period (the peak hour itself plus 15 minutes either side) with a synthesised peak flow profile within this time, which is robust. The results of the assessment are summarised in Table 3.1 with full program output attached at Appendix E. This shows the maximum Ratio of Flow to Capacity (RFC) value, delay and queue per vehicle predicted by the model for each give way manoeuvre during any 15 -minutes within the modelled period.

## Table 3.1: Summary of results of PICADY capacity assessment of Main Road/Haul Road access junction

| Manoeuvre | Weekday pm peak hour |  |  |
| :---: | :---: | :---: | :---: |
|  | RFC | Delay (mins/veh) | Queue (vehs) |
| Egress from Haul Road | 0.046 | 0.16 | 0.0 |
| Main Road northbound <br> ahead + right turn <br> Overall junction delay <br> (mins/veh) | 0.047 | 0.10 | 0.1 |

3.17 Table 3.1 shows that the proposed junction with the Haul Road is expected to operate well within capacity, with maximum RFC values of under 0.1 and so well below the desirable maximum of 0.85 and negligible queuing and delays (a few seconds per vehicle).
3.18 The provision of the access will require an existing lighting column to be relocated. Since site operating hours will be only until 16:30, vehicles would only be entering and leaving the site during darkness during 3 months in the Winter (namely in November, December and January), and the site will be closed for over a week around the Christmas and New Year period. The access will be signed appropriately.

## Vehicle Routing

3.19 Construction vehicles could route to the site via either: the A232 and then south on the A223; or alternatively via the A25 and then north on the A223.

## Wash-down Facilities

3.20 The A223 will be kept free of soils resulting from the movement of tipper wagons on the site. This will be achieved with a wheel cleaning spinner on egress from the site compound and road sweeper(s) at the site access when required.
3.21 In addition, a mobile water bowser will be available on site and will be used to suppress dust arising during dry periods. The regular washing of vehicles and dampening of surfaces and materials in dry conditions, will ensure that dust does not have any significant impact beyond the application site boundaries.

## Construction Vehicle Sizes

3.22 The recovered inert soils would be brought to the site by Woodland Environmental using 4-axle tipper spoil wagons.
3.23 A variety of plant may be needed during the course of operations, although it is unlikely that all of the plant will be required at the same time. It is proposed that a tracked bulldozer and/or excavator suitable for grading of inert spoils will remain on site for the
duration of the tipping operations. At other times a dumper truck and a 360 degree excavator will be required and these would be brought in or hired as appropriate.
3.24 All plant and machinery required for the earthworks operations will be stationed on the course itself.

## Construction Schedule

3.25 The duration of the construction phase is anticipated to be in the order of 18 months, depending on the availability of suitable inert soils, and also restricted hours of operation due to adverse weather conditions, which may result in the period being extended to 24 months. This excludes the construction and disposal of the haul road and site compound.
3.26 Normal operating hours for the fill importation will be restricted to 09:30-16:30 Mondays to Fridays, outside of the busiest highway network morning and evening peak periods, which can be enforced by means of a planning condition. These restrictions on operating times seek to negate the need for a right-turn lane at the site access. The operating hours also avoid weekends when use of the PRoWs is highest, and when residents of houses on Main Road near to the proposed junction with the haul road are most likely to be at home, so minimising disturbance. There will be no construction activity in the evenings, overnight or early mornings which again are sensitive periods when residents are most likely to be at home.
3.27 In terms of construction vehicle movements, it is anticipated that the site will receive 70 deliveries per weekday, which equates to a total of 350 deliveries per week and 10 an hour on average.

## On-Site Management Strategy

3.28 Between 4 and 8 WE employees would be on-site every day of construction. An employee would be present at all times when the site is open to accept imported soils.
3.29 Site control during the landscape works will be undertaken by an experienced member of WE and all vehicles delivering fill to the site would report to him. Records would be kept of all loads deposited at the site and this would be retained by the site supervisor. Records would be available for inspection by officers of the appropriate regulatory authority as necessary.
3.30 A representative of WE will be available for liaison with LBB should issues arise during the works.
3.31 In order to limit congestion on-site, deliveries of materials will be co-ordinated to ensure that vehicle arrive on a staggered basis.

## Overhang of the Public Highway

3.32 There would be no overhang of the public highway by cranes etc as part of the construction works.

## Proposed Hoarding

3.33 If LBB sees fit, hoarding is proposed around the works to limit any instances of dust entering the public highway. This would be secured by means of a planning condition.

## Pedestrian, Cyclist and Equestrian Safety

3.34 As identified earlier, the proposed temporary junction arrangement at Main Road includes footways around its radii to provide safe connections to the PRoW for pedestrians.
3.35 The PRoW routes would be retained as existing and there would be a suitable buffer between these and the haul road, with protective fencing provided as necessary to ensure safety to the public.

At the points where the haul road crosses a PRoW, a safe crossing area with good visibility will be provided on the approaches, with vegetation cut back as necessary, as well as warning signs to the public and lorry drivers. The speed limit on the road will be 10 mph , and with twoway traffic permitted along the length of the road HGVs will be able to travel at this speed continuously so heavy braking will not be ncessary. Speed reducing ramps could be provided at points where the road crosses PRoWs if LBB considers this necessary.
3.37 The golf course will remain open to the public for the duration of the construction works. During the operations all necessary steps would be taken to ensure that the public using the golf course are fully aware of the operations and are safe from manoeuvring vehicles. This will take the form of protective fencing around the works and appropriately located warning signs to the public and lorry drivers.
3.38 Possible conflicts between construction traffic and pedestrians, cyclists and equestrians will be minimised through on-site management. If required, trained banksmen would supervise reversing vehicles. As highlighted above, during site operating hours, a banksman would be deployed at the points where the existing PRoWs cross the haul road to ensure the safety of walkers, cyclists and equestrians. As Plate 3 shows, only one access into the site is now to be provided across Bridleway BR277 (the easternmost of the two originally proposed) in order to limit the impact on the PRoWs.
3.39 LBB has requested that WE indemnify the Council against any claims for injury or damage that may arise as a result of the proposed crossing of the existing public rights of way by the haul road. WE
has confirmed that this could be dealt with by means of a Unilateral Undertaking.

## Haul Road route construction and decommissioning

3.40 The initial section of the Haul Road will be surfaced with concrete to minimise dust during the dry summer months.
3.41 WE is prepared to accept a condition requiring the route of the haul road to be made good following the cessation of its use.

### 4.0 SUMMARY AND CONCLUSIONS

4.1 This Revised Construction Traffic Management Statement has been prepared for submission to LBB to provide additional information in support of the planning application for the upgrading and modernisation of the Cherry Lodge Golf Club, Biggin Hill.
4.2 The works will comprise the importation of recovered inert soils brought to the site by WE using 4 -axle tipper spoil wagons. The duration of the construction phase is anticipated to be in the order of 18-24 months, depending on the availability of suitable inert soils and weather conditions. Normal operating hours for the fill importation will be 09:30-16:30 Mondays to Fridays, outside of the busiest highway network morning and evening periods.
4.3 The temporary haul road is proposed to connect to Main Road via a new priority ' $T$ ' junction arrangement. The proposed junction arrangement respects the PRoWs and includes footways around its radii to provide alternative connections to these for walkers, whilst the Byway/Bridleway connection to Main Road is retained as a vehicular crossover. A gate will be provided behind the point where Bridleway BR275B crosses and will be closed outside of site operating hours to ensure no use by unauthorised vehicles.
4.4 Vehicle flow and speed surveys have been undertaken on Main Road to inform junction visibility splay requirements, which are $2.4 \mathrm{~m} x$ 53 m and 57 m looking left (south) and right (north), respectively. The restrictions on operating times seek to negate the need for a right-turn lane at the site access. A safety audit of the proposed junction has been undertaken, which does not highlight any issues which cannot be easily addressed. A robust PICADY capacity assessment, which demonstrates that the junction would operate well within capacity with the expected flows (on the basis of the onerous assumption that 15 HGVs will enter, and 15 will leave, the
site each hour, compared to the 10 expected) has also been undertaken.
4.5 The PRoW routes would be retained as existing and there would be a suitable $10-15 \mathrm{~m}$ wide buffer between these and the haul road, with protective fencing provided to ensure safety to the public. On occasion when the haul road crosses a PRoW, a safe crossing area with good visibility will be provided, as well as warning signs to the public and lorry drivers. A 10 mph speed limit will apply on the haul road, and during site operating hours banksmen will be deployed where it crosses PRoWs to ensure the safety of walkers, cyclists and equestrians.
4.6 The golf course will remain open to the public for the duration of the construction works. During the operations all necessary steps would be taken to ensure that the public using the golf course are fully aware of the operations and are safe from manoeuvring vehicles.


## Appendix A

Woodland Environmental Haul Road Routes Drawing nos 100.23 Rev C and 100.24 Rev C



## Appendix B

Public Rights of Way Map


Appendix C

Traffic Speed Survey Results

## Countsequential



Speed Surveys at

Main Road, Biggin Hill

Countsequential Ltd
3 Lewes Road - Bromley
Kent - BR1 2RN

T 02088195809
F 02088195617
M 07973280966


Main Road, Biggin Hill - Point of survey photos


## C. Countsequential

## SPEED SURVEY RESULTS:

## MAIN ROAD, BIGGIN HILL

TUESDAY 02²d JUNE 2009

## C. Countsequential

LOCATION : MAIN ROAD, BIGGIN HILL (OPPOSITE NO. 344)

WEATHER : DRY

CARRIAGEWAY : SINGLE ROADWORKS : NONE

|  |  |  |  |
| :---: | :---: | :---: | :---: |
|  | NORTHBOUND | SOUTHBOUND |  |
| SPEED (mph) | NUMBER OF VEHICLES | NUMBER OF VEHICLES | SPEED (kph) |
| 10 |  |  | 16 |
| 11 |  |  | 18 |
| 12 |  |  | 19 |
| 13 |  |  | 21 |
| 14 |  |  | 23 |
| 15 |  |  | 24 |
| 16 |  |  | 26 |
| 17 |  |  | 27 |
| 18 |  |  | 29 |
| 19 |  |  | 31 |
| 20 |  |  | 32 |
| 21 |  |  | 34 |
| 22 |  |  | 35 |
| 23 |  |  | 37 |
| 24 |  |  | 39 |
| 25 |  |  | 40 |
| 26 | 2 | 1 | 42 |
| 27 | 1 | 3 | 43 |
| 28 | 5 | 5 | 45 |
| 29 | 8 | 6 | 47 |
| 30 | 8 | 6 | 48 |
| 31 | 14 | 10 | 50 |
| 32 | 8 | 5 | 51 |
| 33 | 7 | 8 | 53 |
| 34 | 13 | 16 | 55 |
| 35 | 5 | 7 | 56 |
| 36 | 14 | 5 | 58 |
| 37 | 4 | 8 | 60 |
| 38 | 1 | 4 | 61 |
| 39 | 3 | 4 | 63 |
| 40 |  | 3 | 64 |
| 41 | 5 | 2 | 66 |
| 42 |  | 2 | 68 |
| 43 | 1 | 2 | 69 |
| 44 |  | 1 | 71 |
| 45 |  | 1 | 72 |
| 46 | 1 |  | 74 |
| 47 |  |  | 76 |
| 48 |  | 1 | 77 |
| 49 |  |  | 79 |
| 50 |  |  | 80 |
| O A | $1 \square$ | $1 \square$ |  |
| $\square \mathrm{t} \square \mathrm{ile}$ [dr $\square$ $\square \mathrm{t} \square \square \mathrm{ile} \square \square$ et SSD IDMR $\square \square$ SSD MS $\square 1$ |  | $\square \square$ <br> $\square \square$ <br> $\square \square$ <br> $\square \square$ <br> $\square \square$ | $\begin{aligned} & \square \mathbf{p} \square \\ & \square \mathbf{p} \\ & \square \mathbf{p} \\ & \square \end{aligned}$ |


| LOWEST SPEED | 26 mph | 26 mph |
| :---: | :--- | :--- |
| MEAN SPEED | 33 mph | 34 mph |
| MEDIAN SPEED | 33 mph | 34 mph |
| HIGHEST SPEED | 46 mph | 48 mph |

[^0]** SSD based on Manual for Streets


## C. Countsequential

## SPEED SURVEY RESULTS:

## MAIN ROAD, BIGGIN HILL

FRIDAY 05th JUNE 2009

## C. Countsequential

DATE : 05th JUNE 2009
DAY: FRIDAY

LOCATION : MAIN ROAD, BIGGIN HILL (OPPOSITE NO. 344)
WEATHER : DRY

CARRIAGEWAY : SINGLE ROADWORKS : NONE

|  |  |  |  |
| :---: | :---: | :---: | :---: |
|  | NORTHBOUND | SOUTHBOUND |  |
| SPEED (mph) | NUMBER OF VEHICLES | NUMBER OF VEHICLES | SPEED (kph) |
| 10 |  |  | 16 |
| 11 |  |  | 18 |
| 12 |  |  | 19 |
| 13 |  |  | 21 |
| 14 |  |  | 23 |
| 15 |  |  | 24 |
| 16 |  |  | 26 |
| 17 |  |  | 27 |
| 18 |  |  | 29 |
| 19 |  |  | 31 |
| 20 |  |  | 32 |
| 21 |  | 1 | 34 |
| 22 |  | 1 | 35 |
| 23 |  |  | 37 |
| 24 |  |  | 39 |
| 25 |  |  | 40 |
| 26 |  |  | 42 |
| 27 | 2 | 3 | 43 |
| 28 | 3 | 3 | 45 |
| 29 | 3 | 4 | 47 |
| 30 | 9 | 19 | 48 |
| 31 | 8 | 10 | 50 |
| 32 | 11 | 6 | 51 |
| 33 | 19 | 8 | 53 |
| 34 | 11 | 8 | 55 |
| 35 | 6 | 11 | 56 |
| 36 | 6 | 3 | 58 |
| 37 | 8 | 7 | 60 |
| 38 | 5 | 3 | 61 |
| 39 | 2 |  | 63 |
| 40 | 2 | 6 | 64 |
| 41 |  | 3 | 66 |
| 42 | 3 |  | 68 |
| 43 |  |  | 69 |
| 44 |  | 1 | 71 |
| 45 | 1 | 2 | 72 |
| 46 |  | 1 | 74 |
| 47 |  |  | 76 |
| 48 |  |  | 77 |
| 49 | 1 |  | 79 |
| 50 |  |  | 80 |
| O A | $1 \square$ | $1 \square$ |  |
|  |  |  | $\begin{aligned} & \square \mathbf{p} \square \\ & \square \mathbf{p} \square \\ & \square \mathbf{p} \square \\ & \square \end{aligned}$ |


| LOWEST SPEED | 27 mph | 21 mph |
| :---: | :--- | :--- |
| MEAN SPEED | 34 mph | 33 mph |
| MEDIAN SPEED | 33 mph | 33 mph |
| HIGHEST SPEED | 49 mph | 46 mph |

[^1]** SSD based on Manual for Streets


Appendix D

Stage 1 Road Safety Audit

# Road Safety Audit Stage 1 

## A233 Main Road

Proposed Temporary Access

## Biggin Hill

Date: $9^{\text {th }}$ October 2011
Report produced for: Ardent Consulting Engineers
Report produced by: M \& S Traffic Ltd

## DOCUMENT CONTROL SHEET

| Project Title | A233 Main Road, Biggin Hill |
| :--- | :--- |
|  | Proposed Temporary Access for Cherry Lodge Golf Club |

Report Title Road Safety Audit Stage 1

Revision

Status Final

Reference F990/1/MM

Record of Issue

| Issue | Status | Author | Date | Check | Date | Authorised | Date |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Draft | MM | $05 / 10 / 11$ | BS | $06 / 10 / 11$ | MM | $06 / 10 / 11$ |
| 1 | Final | MM | $09 / 10 / 11$ | BS | $09 / 10 / 11$ | MM | $09 / 10 / 11$ |

Distribution

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| Ardent Consulting Engineers | Matthew Last | - |
|  |  |  |

## CONTENTS

Document Control Sheet ..... 2
Contents ..... 3
1 Introduction ..... 4
2 The Scheme ..... 5
3 Traffic Conditions ..... 6
$4 \quad$ Items raised by the Stage 1 Audit ..... 7
5 Auditors Statement ..... 9
Appendix A List of drawings
Appendix B. Comment location drawing
Appendix C Designer's Response

## 1 INTRODUCTION

1.1 This report describes a Stage 1 Road Safety Audit carried out on a proposed temporary HGV access for the redevelopment of Cherry Lodge Golf Club on the A233 Main Road, Biggin Hill. The Audit was requested by the design organisation, Ardent Consulting Engineers, 4th Floor, Diamond House, 36/38 Hatton Garden, London EC1N 8EB.
1.2 The Audit Team membership was as follows:

Martin Morris PGD, MCIHT, Audit Team Leader
Bryan Shawyer BEng (Hons), MSc, MCIHT, Audit Team Member
1.3 The audit was undertaken in accordance with the audit brief and HD 19/03, The Design Manual for Roads and Bridges. The documents available at the time of the report was compiled are detailed in Appendix A.
1.4 A site visit and inspection was undertaken during the afternoon of the $5^{\text {th }}$ October 2011, weather conditions at the time were dry and overcast. Traffic flows on Main Road were moderate and free flow speeds were also moderate.
1.5 The report has been compiled, only with regard to the safety implications for road users of the layout presented in the supplied drawings. It has not been examined or verified for compliance with any other standards or criteria. This safety audit does not perform any "Technical Check" function on these proposals. It is assumed that the Project Sponsor is satisfied that such a "Technical Check" has been successfully completed prior to requesting this safety audit.
1.6 The auditors have not been informed of any Departures from Standards in this scheme construction.
1.7 All comments and recommendations are referenced to the detailed drawings and the locations have been detailed relating to the plans supplied with the audit brief, Appendix B.
1.8 The Designer's Response to this audit has been included in Appendix C.

## 2 THE SCHEME

2.1 The scheme proposes to construct a temporary HGV access for the redevelopment of Cherry Lodge Golf Club, on the A233 Main Road, Biggin Hill.
2.2 The junction design includes footways around its radii to provide alternative connections to these Public Rights of Way for walkers, whilst the Byway/Bridleway connection to Main Road is retained as a vehicular crossover.

## 3 TRAFFIC CONDITIONS

3.1 This section of the A233 Main Road, Biggin Hill is rural in nature and is fronted by both residential development and local businesses. Main Road performs the role of a local distributor route and is subject to a 30 mph speed restriction. The proposed temporary junction arrangement is located close to the points at which Byway 283 and Bridleway 275B connect to the A233 Main Road.
3.2 Observed traffic flows and speeds on Main Road were moderate.
3.3 There were no movements on the Byway or Bridleway.
3.4 No traffic or pedestrian data was supplied at the time of the audit.

## 4 ITEMS RAISED AT THE STAGE 1

### 4.1 General

4.1.1 No comment.

### 4.2 Local Alignment

### 4.2.1 PROBLEM

Location: Junction of the Access Road and Main Road
Summary: Ponding of surface water could lead to loss of control accidents.
No details of drainage or vertical profiles have been provided for the junction, any ponding on Main Road could lead to loss of control accidents.

## RECOMMENDATION

That drainage details and carriageway profiles be provided at safety audit stage 2.

### 4.3 Junctions

### 4.3.1 PROBLEM

Location: Junction of the Access Road and Main Road.
Summary: Lack of visibility may lead to side impact accidents.
It is proposed that the visibility splays are 57 m and 53 m and are based on a 2 m height above carriageway level. It was noted that from the Construction Traffic Management Statement that the visibility distances from Manual for Streets have been used. It would appear that greater visibility distances in accordance or possibly in excess of the requirements of TD42/95 could be achieved with minimal vegetation trimming.

## RECOMMENDATION

That as the haul route will be used for a $18-24$ month period, with slow moving traffic exiting the junction that consideration be given to increasing the visibility splays.

### 4.3.2 PROBLEM

Location: Junction of the Access Road and Main Road.
Summary: Lack of visibility may lead to side impact accidents.
In the Construction Traffic Management Statement, it is stated that the haul route is to be used exclusively by HGVs. However, it is unclear how this will be enforced and should other traffic egress from the site then the visibility splays would be insufficient.

## RECOMMENDATION

That details be provided, as to how HGV only controls would be introduced or that consideration be given to introduce visibility splays suitable for all vehicle types.

### 4.4 Non Motorised User Provision

4.4.1 No comment.

### 4.5 Road Signs, Carriageway Markings and Lighting

### 4.5.1 PROBLEM

Location: Junction of the Access Road and Main Road.
Summary: Absence of street lighting may lead to accidents during the hours of darkness.
The proposal places the junction where there is an existing street lighting column. No details have been supplied, as to additional lighting or where the removed column is to be repositioned. A reduction in the luminance on Main Road may give rise to accidents during the hours of darkness. Furthermore should the spacing between columns be too great then the current 30 mph speed limit may not apply.

## RECOMMENDATION

That street lighting details be provided at safety audit stage 2.

## 5 AUDITOR TEAM STATEMENT

I certify that this audit has been carried out in accordance with HD 19/03.

## Audit Team Leader

Martin Morris PGD, MCIHT
M \& S Traffic Ltd
Aeolos House
32 Hamelin Road
Signed $\qquad$

Date $\qquad$
Gillingham
Kent ME7 3EX

## Audit Team Member

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Gillingham
Kent ME7 3EX

## APPENDIX A

List of Drawings submitted for auditing:

- Drawing No. F990-003: Proposed Temporary Access.
- Report No. F990-02 Cherry Lodge golf Club, Construction Traffic Management Statement.


## APPENDIX B

Plan attached showing the locations of the problems identified as part of this audit (location numbers refer to paragraph numbers in the report).


APPENDIX C - DESIGNER'S RESPONSE

## DOCUMENT CONTROL SHEET

| REV | ISSUE PURPOSE | AUTHOR | CHECKED | APPROVED | DATE |
| :--- | :--- | :---: | :---: | :---: | :---: |
|  | $1^{\text {st }}$ Draft for project team <br> review | ML | SAF | ML | $07 / 10 / 11$ |
|  | Final | ML | SAF | ML | $09 / 10 / 11$ |
|  |  |  |  |  |  |


| Audit <br> Item <br> No. | Problem <br> accepted <br> (yes/no) | Recommended <br> measure <br> accepted <br> (yes/no) | Alternative Measures <br> (describe) | Alternative <br> measures <br> accepted by <br> Audit Team <br> (yes/no) |  |
| :---: | :---: | :---: | :--- | :--- | :--- |
| 4.2 .1 | Yes | Yes | N/A |  |  |
| 4.3 .1 | Yes | Yes | Visibility splay "Y" distance requirements are <br> based on Stopping Sight Distances commensurate <br> with observed $85^{\text {th }}$ percentile speeds derived from <br> the Manual for Streets, as agreed with LBB. If <br> LBB consider that the "Y" distances should be <br> increased to 90m (for a road with a 30mph speed <br> limit) in accordance with TD 42/95 then this could <br> be achieved by cutting back more of the exising <br> hedgerow. |  |  |
| 4.3 .2 | Yes |  | Yes | Visibility splay requirements will be based on <br> standard car driver eye heights of $1.05 m$ with the | Yes |
| 4.5 .1 | Yes |  | hedgerow trimmed above this height. In addition, <br> gates will be provided behind the route of the <br> public footpath which will be closed outside of site <br> operating hours. |  |  |

## Appendix E

Results of traffic survey on Main Road and PICADY capacity assessment of proposed junction with Haul Road

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|}
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11.1 <br>
\hline 0200 \& 6 \& 0 \& 5 \& 0 \& 1 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& \& 0200 \& 0 \& 0 \& 0 \& 0 \& 0 \& 1 \& 1 \& 2 \& 1 \& 1 \& 0 \& 0 \& 0 \& 0 \& 42.9 - \& \& 4 \& 66.7 \& 2 \& 33.3 \& 0 \& 0 <br>
\hline 0300 \& 5 \& 0 \& 3 \& 0 \& 2 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& \& 0300 \& 0 \& 0 \& 0 \& 0 \& 0 \& 1 \& 1 \& 2 \& 1 \& 0 \& 0 \& 0 \& 0 \& 0 \& 40.5 . \& \& \& 60 \& 1 \& 20 \& 0 \& 0 <br>
\hline 0400 \& 19 \& 1 \& 16 \& 0 \& 2 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& \& 0400 \& 0 \& 0 \& 0 \& 0 \& 2 \& 3 \& 7 \& 3 \& 2 \& 2 \& 0 \& 0 \& 0 \& 0 \& 39.2 \& 46.8 \& 7 \& 36.8 \& 4 \& 21.1 \& 1 \& 5.3 <br>
\hline 0500 \& 46 \& 2 \& 38 \& 0 \& 5 \& 1 \& 0 \& 0 \& 0 \& 0 \& 0 \& \& 0500 \& 0 \& 0 \& 0 \& 0 \& 4 \& 5 \& 10 \& 13 \& 12 \& 2 \& 0 \& 0 \& 0 \& 0 \& 40.7 \& 47 \& 27 \& 58.7 \& 10 \& 21.7 \& 0 \& <br>
\hline 0600 \& 159 \& 4 \& 137 \& 0 \& 14 \& 3 \& 0 \& 0 \& 0 \& 1 \& 0 \& \& 0600 \& 0 \& 0 \& 1 \& 1 \& 32 \& 35 \& 45 \& 29 \& 11 \& 5 \& 0 \& 0 \& 0 \& 0 \& 36.3 \& 42.9 \& 45 \& 28.3 \& 11 \& 6.9 \& 2 \& 1.3 <br>
\hline 0700 \& ${ }^{412}$ \& 10 \& ${ }^{358}$ \& 1 \& ${ }^{40}$ \& 1 \& 1 \& 1 \& 0 \& 0 \& 0 \& \& 0700 \& 1 \& 1 \& 3 \& 10 \& 49 \& 154 \& ${ }^{143}$ \& 39 \& 9 \& 3 \& 0 \& 0 \& 0 \& 0 \& 34.6 \& 39.1 \& 51 \& ${ }^{12.4}$ \& 7 \& 1.7 \& 1 \& 0.2 <br>
\hline \& ${ }^{421}$ \& 4 \& ${ }^{380}$ \& 2 \& ${ }^{31}$ \& 1 \& 1 \& 0 \& 1 \& 1 \& 0 \& \& 0800 \& 0 \& 7 \& 10 \& 13 \& 59 \& 158 \& ${ }^{133}$ \& 32 \& 9 \& 0 \& 0 \& 0 \& 0 \& 0 \& 33.5 \& 38.9 \& 41 \& 9.7 \& 4 \& \& 0 \& <br>
\hline 0900 \& 327 \& 1 \& 281 \& 0 \& 39 \& 2 \& 2 \& 2 \& 0 \& 0 \& 0 \& \& 0900 \& 0 \& 1 \& 2 \& 10 \& 63 \& 139 \& 83 \& 22 \& 7 \& 0 \& 0 \& 0 \& 0 \& 0 \& 33.6 \& 38.3 \& 29 \& 8.9 \& 4 \& 1.2 \& 0 \& <br>
\hline 1000 \& 291 \& 1 \& 254 \& 1 \& 32 \& 0 \& 1 \& 1 \& 1 \& 0 \& 0 \& \& 1000 \& 1 \& 1 \& 1 \& 8 \& 70 \& 139 \& 58 \& 10 \& 1 \& 2 \& 0 \& 0 \& 0 \& 0 \& 32.2 \& 36.2 \& 13 \& 4.5 \& 3 \& 1 \& 0 \& 0 <br>
\hline 1100 \& 263 \& 1 \& 229 \& 2 \& 29 \& 0 \& 2 \& 0 \& 0 \& 0 \& 0 \& \& 1100 \& 0 \& 0 \& 2 \& 3 \& 39 \& 109 \& 75 \& 25 \& 8 \& 2 \& 0 \& 0 \& 0 \& 0 \& 34.6 \& 39.6 \& 35 \& 13.3 \& 8 \& 3 \& 0 \& <br>
\hline 1200 \& 295 \& 3 \& 265 \& 0 \& 26 \& 1 \& 0 \& 0 \& 0 \& 0 \& 0 \& \& 1200 \& 0 \& 1 \& 1 \& 2 \& 45 \& 144 \& 82 \& 17 \& 2 \& 1 \& 0 \& 0 \& 0 \& 0 \& 33.6 \& 37.8 \& 20 \& 6.8 \& \& 0.3 \& 0 \& <br>
\hline 1300 \& 269 \& 2 \& 231 \& 1 \& 33 \& 0 \& 0 \& 0 \& 2 \& 0 \& 0 \& \& 1300 \& 0 \& 0 \& 5 \& 11 \& 50 \& 118 \& 61 \& 19 \& 3 \& 2 \& 0 \& 0 \& 0 \& 0 \& 33.1 \& 38.5 \& 24 \& 8.9 \& 5 \& 1.9 \& 1 \& 0.4 <br>
\hline 1400 \& 331 \& 6 \& 277 \& 4 \& 38 \& 0 \& 4 \& 0 \& 1 \& 0 \& 1 \& \& 1400 \& 0 \& 0 \& 1 \& 6 \& 67 \& 140 \& 87 \& 27 \& 2 \& 1 \& 0 \& 0 \& 0 \& 0 \& 33.5 \& 38.3 \& 30 \& 9.1 \& 2 \& 0.6 \& 0 \& <br>
\hline 1500 \& 386 \& 11 \& 327 \& 1 \& 44 \& 0 \& 0 \& 0 \& 1 \& 2 \& 0 \& \& 1500 \& 0 \& 1 \& 2 \& 17 \& 62 \& 147 \& 122 \& 29 \& 6 \& 0 \& 0 \& 0 \& 0 \& O \& 33.7 \& 38.3 \& 35 \& 9.1 \& \& \& 0 \& <br>
\hline 1600 \& 507 \& 6 \& 451 \& 2 \& 41 \& 1 \& 2 \& 0 \& 2 \& 0 \& 2 \& \& 1600 \& 0 \& 0 \& 5 \& 15 \& 72 \& 251 \& 133 \& 23 \& 6 \& 2 \& 0 \& 0 \& 0 \& 0 \& 33.4 \& 37.4 \& 31 \& 6.1 \& 7 \& 1.4 \& 0 \& <br>
\hline 1700 \& 574 \& 12 \& 527 \& 0 \& 31 \& 2 \& 0 \& 0 \& 2 \& 0 \& 0 \& \& 1700 \& 0 \& 2 \& 7 \& 5 \& 53 \& 278 \& 183 \& 39 \& 6 \& 0 \& 1 \& 0 \& 0 \& \& 34.2 \& 38.5 \& 46 \& 8 \& 3 \& 0.5 \& 1 \& 0.2 <br>
\hline 1800 \& 363 \& 3 \& 330 \& 4 \& 24 \& 0 \& 1 \& 0 \& 0 \& 0 \& 1 \& \& 1800 \& 1 \& 1 \& 1 \& 2 \& ${ }^{43}$ \& 117 \& 140 \& 50 \& 6 \& 2 \& 0 \& 0 \& 0 \& 0 \& 35.2 \& 40 \& 58 \& 16 \& 6 \& 1.7 \& 0 \& <br>
\hline 1900 \& 242 \& 4 \& ${ }^{223}$ \& 1 \& 13 \& 0 \& 0 \& 0 \& 1 \& 0 \& 0 \& \& 1900 \& 0 \& 0 \& 0 \& 0 \& 26 \& 97 \& 90 \& 23 \& 5 \& 1 \& 0 \& 0 \& 0 \& 0 \& 35.3 \& 38.9 \& 29 \& 12 \& 5 \& 2.1 \& 0 \& <br>
\hline 2000 \& 149 \& 1 \& 141 \& 0 \& 6 \& 0 \& 0 \& 0 \& 1 \& 0 \& 0 \& \& 2000 \& 0 \& 0 \& 0 \& 2 \& 15 \& 51 \& 48 \& 21 \& 8 \& 3 \& 1 \& - \& 0 \& 0 \& 36.2 \& 42.1 \& 33 \& 22.1 \& 9 \& 6 \& 1 \& 0.7 <br>
\hline 2100 \& 109 \& 4 \& 101 \& 1 \& 3 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& \& 2100 \& 0 \& 0 \& 0 \& 0 \& 5 \& 45 \& 34 \& 19 \& 5 \& 1 \& 0 \& 0 \& 0 \& 0 \& 36.4 \& 41.6 \& 25 \& 22.9 \& 5 \& 4.6 \& 1 \& 0.9 <br>
\hline 2200 \& 85 \& 0 \& 83 \& 0 \& 2 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& \& 2200 \& 0 \& 0 \& 0 \& 2 \& 7 \& 27 \& 29 \& 15 \& 4 \& 1 \& 0 \& 0 \& 0 \& 0 \& 36.5 \& 41.8 \& 20 \& 23.5 \& 4 \& 4.7 \& 1 \& 1.2 <br>
\hline 2300 \& \& \& \& 0 \& \& 0 \& \& \& \& 0 \& 0 \& \& 2300 \& 0 \& 0 \& 0 \& 0 \& 4 \& 10 \& 22 \& 9 \& 6 \& 2 \& 1 \& 0 \& 0 \& \& 38.7 \& 45.4 \& 18 \& 33.3 \& \& 11.1 \& 2 \& <br>
\hline 07-19 \& 4439 \& 60 \& 3910 \& 18 \& 408 \& 8 \& 14 \& 4 \& 10 \& 3 \& 4 \& \& 07-19 \& 3 \& 15 \& 40 \& 102 \& 672 \& 1894 \& 1300 \& 332 \& 65 \& 15 \& 1 \& 0 \& 0 \& 0 \& 33.8 \& 38.5 \& 413 \& 9.3 \& 54 \& 1.2 \& 3 \& 0.1 <br>
\hline 06-22 \& 5098 \& 73 \& 4512 \& 20 \& 444 \& 11 \& 14 \& 4 \& 12 \& 4 \& 4 \& \& $06-22$ \& 3 \& 15 \& 41 \& 105 \& 750 \& 2122 \& 1517 \& 424 \& 94 \& 25 \& 2 \& 0 \& 0 \& 0 \& 34.1 \& 38.7 \& 545 \& 10.7 \& 84 \& 1.6 \& 7 \& 0.1 <br>
\hline 06-00 \& 5237 \& 75 \& 4644 \& 20 \& 449 \& 11 \& 14 \& 4 \& 12 \& 4 \& 4 \& \& 06-00 \& 3 \& 15 \& 41 \& 107 \& 761 \& 2159 \& 1568 \& 448 \& 104 \& 28 \& 3 \& 0 \& 0 \& 0 \& 34.2 \& 38.9 \& 583 \& 11.1 \& 94 \& 1.8 \& 10 \& 0.2 <br>
\hline 00-00 \& 5339 \& 78 \& 4730 \& 20 \& 461 \& 12 \& 14 \& 4 \& 12 \& 4 \& 4 \& \& 00.00 \& 3 \& 15 \& 41 \& 107 \& 769 \& 2176 \& 1593 \& 472 \& 124 \& 34 \& 5 \& 0 \& 0 \& 0 \& 34.3 \& 38.9 \& 635 \& 11.9 \& 116 \& 2.2 \& 14 \& 0.3 <br>
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\end{tabular}

| Time | Total | $\underset{\substack{\text { cls } \\ 1}}{ }$ | $\underset{\substack{\text { Cls } \\ 2}}{ }$ | ${ }_{\substack{\text { Cls } \\ 3}}$ | ${ }_{4}^{\text {Cls }}$ | $\begin{gathered} \mathrm{Cls} \\ 5 \end{gathered}$ | $\underset{6}{\mathrm{Cls}}$ | $\underset{7}{\text { Cls }}$ | $\underset{8}{\mathrm{Cls}}$ | $\underset{9}{\mathrm{Cls}}$ | $\begin{aligned} & \text { Cls } \\ & 10 \end{aligned}$ | Fix1 | Time | $\begin{gathered} \text { Vbin } \\ 0 \\ 10 \end{gathered}$ | $\begin{gathered} \text { Vbin } \\ 10 \\ 15 \end{gathered}$ | $\begin{aligned} & \text { Vbin } \\ & 15 \\ & 20 \end{aligned}$ | $\begin{aligned} & \text { Vbin } \\ & 20 \\ & 25 \end{aligned}$ | $\begin{aligned} & \text { Vinn } \\ & 25 \\ & 30 \end{aligned}$ | $\begin{gathered} \text { Vbin } \\ 30 \\ 35 \end{gathered}$ | $\begin{aligned} & \text { Vbin } \\ & 35 \\ & 40 \end{aligned}$ | $\begin{aligned} & \text { Vbin } \\ & 40 \\ & 45 \end{aligned}$ | $\begin{aligned} & \text { Vbin } \\ & 45 \\ & 50 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Vbin } \\ & 50 \\ & 60 \end{aligned}$ | $\begin{aligned} & \text { Vbin } \\ & 60 \\ & 70 \end{aligned}$ | $\begin{aligned} & \text { Vinn } \\ & 70 \\ & 80 \end{aligned}$ | $\begin{gathered} \text { Vinn } \\ 80 \\ 90 \end{gathered}$ | $\begin{gathered} \text { Vbin } \\ 90 \\ 100 \end{gathered}$ | Mean | $\begin{gathered} \mathrm{vpp}_{8}^{85} \\ 85 \end{gathered}$ | $\begin{aligned} & \text { >PSL } \\ & 40 \end{aligned}$ | $\begin{aligned} & \text { PPSL\% } \\ & 40 \end{aligned}$ | $\begin{gathered} >\mathrm{SL} L 1 \\ 46 \\ \text { ACPO } \end{gathered}$ | $\begin{aligned} & \text { >SLL\% } \\ & \text { 4CPO } \end{aligned}$ | $\begin{gathered} >\mathrm{SLL} \\ 55 \\ 55 \\ \text { DFT } \end{gathered}$ | $\begin{gathered} >\mathrm{SLL} \% \\ 55 \\ \text { DFT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0000 | 17 | 0 | ${ }^{16}$ | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0000 | 0 | 0 | 0 | 0 | 1 | ${ }^{6}$ | 4 | 2 | 2 | 0 | 2 | 0 | 0 | 0 | 39.7 | 45.4 | ${ }_{5}$ | 35.3 | ${ }^{3}$ | 17.6 | ${ }^{2}$ |  |
| 0100 0200 | 9 | 0 | 8 | 0 | 1 | 0 | 0 | 0 | 0 0 | 0 0 | 0 0 |  | $\begin{aligned} & 000 \\ & 0200 \\ & 020 \end{aligned}$ | 0 | 0 | 0 | 0 | 1 | 1 | ${ }_{1}^{2}$ | 2 | ${ }_{1}^{2}$ | 1 | 0 | 0 | 0 | 0 | 41.8 - |  | 5 | ${ }_{65.7}^{55.6}$ | 2 | ${ }_{33.3}^{22.2}$ | 1 |  |
| 0300 | 5 | 0 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0300 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 40.5 - |  |  | 60 | 1 | 20 | 0 |  |
| 0400 | 19 | 1 | 16 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0400 | 0 | 0 | 0 | 0 | 2 | 3 | 7 | 3 | 2 | 2 | 0 | 0 | 0 | 0 | 39.2 | 46.8 |  | 36.8 | 4 | 21.1 |  |  |
| 0500 | 46 | 2 | 38 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 0 |  | 0500 | 0 | 0 | 0 | 0 | 4 | 5 | 10 | 13 | 12 | 2 | 0 | 0 | 0 | 0 | 40.7 | 47 | 27 | 58.7 | 10 | 21.7 | 0 |  |
| 0600 | 159 | 4 | 137 | 0 | 14 | 3 |  | 0 | 0 | 1 | 0 |  | 0600 | 0 | 0 | 1 | 1 | 32 | 35 | 45 | 29 | 11 | 5 | 0 | 0 | 0 | 0 | 36.3 | 42.9 | 45 | 28.3 | 11 | 6.9 | ${ }^{2}$ |  |
| 0700 | 412 | 10 | 358 | 1 | 40 | 1 | 1 | 1 | 0 | 0 | 0 |  | 0700 | 1 | 1 |  | 10 | 49 | 154 | 143 | 39 | 9 | 3 | 0 | 0 | 0 | 0 | 34.6 | 39.1 | 51 | 12.4 | 7 | 1.7 | 1 |  |
| 0800 | ${ }^{421}$ | 1 | 380 | 2 | 31 | 1 | 1 | 0 | 1 | 1 | 0 |  | 0800 | 0 | 7 | 10 | ${ }^{13}$ | 59 | 158 | ${ }^{133}$ | ${ }^{32}$ | 9 | 0 | 0 | 0 | 0 | 0 | 33.5 | 38.9 | ${ }^{41}$ | 9.7 | + | , | 0 |  |
| 0900 | 327 | 1 | 281 | 0 | 39 | 2 | 2 | 2 | 0 | 0 | 0 |  | 0900 | 0 | 1 | 2 | 10 | ${ }^{63}$ | 139 | 83 | 22 | 7 | 0 | 0 | 0 | 0 | 0 | 33.6 | 38.3 | 29 | 8.9 | 4 | 1.2 | 0 |  |
| 1000 1100 | 291 263 | 1 | 254 229 | 1 | 32 29 29 | 0 | 1 | 1 | 1 | 0 | ${ }_{0}^{0}$ |  | 1000 1100 | 1 | 1 | 1 | 8 3 | 70 39 | 139 109 | 58 75 | 10 25 25 | 1 | 2 | 0 | 0 | 0 | 0 | 32.2 34.6 | 36.2 39.6 | 13 35 | 4.5 13.3 | 3 <br> 8 | 1 3 | 0 |  |
| 1100 1200 | 263 295 | 1 | 229 265 | $\stackrel{2}{0}$ | 29 26 | ${ }_{1}$ | 2 | 0 | 0 | 0 | 0 0 |  | 1100 1200 | 0 | ${ }_{1}$ | $\stackrel{2}{1}$ | 2 | 39 45 | 109 144 | 75 82 | 25 17 | 2 | $\stackrel{2}{1}$ | 0 | 0 | 0 | 0 | 34.6 33.6 | 39.6 37.8 | 35 20 | 13.3 6.8 | 8 | 0.3 | 0 |  |
| 1300 | 269 | 2 | 231 | 1 | 33 | 0 | 0 | 0 | 2 | 0 | 0 |  | 1300 | 0 | 0 | 5 | 11 | 50 | 118 | 61 | 19 | 3 | 2 | 0 | 0 | 0 | 0 | 33.1 | 38.5 | 24 | 8.9 | 5 | 1.9 | 1 |  |
| 1400 | 331 | 6 | 277 | 4 | 38 | 0 | 4 | 0 | 1 | 0 | 1 |  | 1400 | 0 | 0 | 1 | ${ }^{6}$ | 67 | 140 | 87 | 27 | 2 | 1 | 0 | 0 | 0 | 0 | 33.5 | 38.3 | 30 | 9.1 | 2 | 0.6 | 0 |  |
| 1500 | ${ }^{386}$ | 11 | 327 | 1 | 44 | 0 | 0 | 0 | 1 | 2 | 0 |  | 1500 | 0 | 1 | 2 | 17 | 62 | 147 | 122 | 29 |  | 0 | 0 | 0 | 0 | 0 | 33.7 | ${ }^{38.3}$ | ${ }^{35}$ | 9.1 | 4 | 1 |  |  |
| 1600 | 507 | 6 | 451 | 2 | ${ }^{41}$ | 1 | 2 | 0 | 2 | 0 | 2 |  | 1600 | 0 | 0 | 5 | 15 | 72 | 251 | ${ }^{133}$ | ${ }^{23}$ | 6 | 2 | 0 | 0 | 0 | 0 | 33.4 | 37.4 | 31 | 6.1 | 7 | 1.4 | 0 |  |
| 1700 1800 | 574 363 | 12 3 | 527 330 | ${ }_{4}$ | 31 24 | ${ }_{0}^{2}$ | ${ }_{1}$ | 0 | 2 | 0 | ${ }_{1}^{0}$ |  | 1700 1800 | 0 | ${ }_{1}$ | 7 | ${ }_{2}$ | ${ }_{43}^{53}$ | 278 117 | 183 140 | 39 50 | 6 | ${ }_{2}$ | 1 | 0 | 0 | 0 | ${ }^{34.2}$ | 38.5 | 46 58 | 16 | 3 | 0.5 | 1 |  |
| 1900 | 342 242 | 4 | ${ }_{223}^{323}$ | 1 | ${ }_{13}^{24}$ | 0 | 0 | 0 | 1 | 0 | 0 |  | 1900 | 0 | 0 | 1 | ${ }_{0}$ | 43 26 | 117 97 | 140 90 | ${ }^{50}$ | ${ }^{6}$ | ${ }_{1}$ | 0 | 0 | 0 | 0 | ${ }_{35.3}^{35.2}$ | 48.9 | 58 29 | 16 12 | ${ }_{6}^{6}$ | 2.1 | 0 |  |
| 2000 | 149 | 1 | 141 | 0 | 6 | 0 | 0 | 0 | 1 | 0 | 0 |  | 2000 | 0 | 0 | 0 | 2 | 15 | 51 | 48 | 21 | 8 | 3 | 1 | 0 | 0 | 0 | 36.2 | 42.1 | 33 | 22.1 |  | 6 | 1 |  |
| 2100 | 109 | 4 | ${ }^{101}$ | 1 |  |  | 0 | 0 | 0 | 0 |  |  | 2100 | 0 | 0 | 0 | 0 | 5 | 45 | 34 | 19 | 5 | 1 | 0 | 0 | 0 | 0 | 36.4 | 41.6 | 25 | 22.9 | 5 | 4.6 | 1 |  |
| 2200 2300 | 85 54 | 2 | 83 49 |  | 2 | 0 0 | 0 | 0 | 0 | 0 | 0 |  | 2200 2300 | ${ }_{0}^{0}$ | ${ }_{0}^{0}$ | 0 | ${ }_{0}^{2}$ | 7 | 27 10 | 29 22 | 15 9 | ${ }_{6}^{4}$ | 1 | ${ }_{1}^{0}$ | 0 | 0 | 0 | 36.5 38.7 | 41.8 45.4 | 20 18 | ${ }_{33.3}^{23.5}$ | 4 6 | ${ }_{11.1}^{4.7}$ | 2 |  |



Grand Total


| Time | Total | $\underset{\substack{\text { cls } \\ 1}}{ }$ | $\underset{2}{\text { cls }}$ | ${ }_{3}$ | $\mathrm{Cls}_{4}$ | ${ }_{c}^{C l s}$ | $\underset{\substack{\text { Cls }}}{ }$ | $\mathrm{Cls}_{7}$ | ${ }_{8}^{\text {cls }}$ | $\underset{9}{\text { Cls }}$ | ${ }_{\text {Cls }}$ | Fix1 | Time | $\begin{gathered} \text { Vbin } \\ 0 \\ 10 \end{gathered}$ | $\begin{gathered} \text { Vbin } \\ 10 \\ 15 \end{gathered}$ | $\begin{gathered} \text { Vbin } \\ 15 \\ 20 \end{gathered}$ | $\begin{aligned} & \text { Vbin } \\ & 20 \\ & 25 \end{aligned}$ | $\begin{gathered} \text { Vbin } \\ 25 \\ 30 \end{gathered}$ | $\begin{aligned} & \text { Vbin } \\ & 30 \\ & 35 \end{aligned}$ | $\begin{gathered} \text { Vbin } \\ 35 \\ 40 \end{gathered}$ | $\begin{aligned} & \text { Vbin } \\ & 40 \\ & 45 \end{aligned}$ | $\begin{gathered} \text { Vbin } \\ 45 \\ 50 \end{gathered}$ | $\begin{aligned} & \text { Vbin } \\ & 50 \\ & 60 \end{aligned}$ | $\begin{aligned} & \text { Vbin } \\ & 60 \\ & 70 \end{aligned}$ | $\begin{gathered} \text { Vinn } \\ 70 \\ 80 \end{gathered}$ | $\begin{gathered} \text { Vbin } \\ 80 \\ 90 \end{gathered}$ | $\begin{gathered} \text { Vbin } \\ 90 \\ 100 \end{gathered}$ | Mean | $\begin{gathered} \mathrm{vpp}_{85}^{85} \\ 85 \end{gathered}$ | $\begin{aligned} & >\text { PSLL } \\ & 40 \end{aligned}$ | ${ }^{>P S L L \%}$ | $\begin{gathered} \text { >SL1 } \\ \text { 46 } \\ \text { ACPO } \end{gathered}$ | $\begin{aligned} & \text { PSLL } \% \\ & 46 \\ & \text { ACPO } \end{aligned}$ | $\begin{aligned} & \text { SSL2 } \\ & 55 \\ & \text { DFT } \end{aligned}$ | $\begin{gathered} \text { SLL2\% } \\ 55 \\ \text { 5FT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0000 | 8 | 1 | 6 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0000 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 40.2 - |  | 5 | 62.5 | 0 | 0 | 0 |  |
| 0100 | 8 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0100 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 41.5 - |  | 5 | ${ }^{62.5}$ | 1 | 12.5 | 0 | 0 |
| 0200 | 4 | 1 | ${ }^{3}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0200 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 48.6 - |  | 4 | 100 | 2 | 50 | 1 |  |
| 0300 | 10 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0300 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 0 | 4 | 0 | 0 | 0 | 0 | 44.7 - |  | 7 | 70 | 4 | 40 | 1 | 10 |
| 0400 | 15 | 0 | 13 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 3 | 3 | 1 | 2 | 0 | 0 | 0 | 43.7 | 57.7 | 9 | 60 | 5 | 33.3 | 3 |  |
| 0500 | 48 | 1 | 39 | 0 | 7 | 1 |  | 0 | 0 | 0 | 0 |  | 0500 | 0 | 0 | 0 | 0 | 3 | 8 | 8 | 12 | 13 | 4 | 0 | 0 | 0 | 0 | 41.5 | 49 | 29 | 60.4 | 15 | 31.3 | 1 | 2.1 |
| 0600 | 185 | 4 | 150 | 0 | 28 | 1 | 2 | 0 | 0 | 0 | 0 |  | 0600 | 0 | 0 | 2 | 0 | 1 | 20 | 64 | 61 | 24 | 13 | 0 | 0 | 0 | 0 | 40.8 | 45.6 | 98 | 53 | 28 | 15.1 | 2 | 1.1 |
| 0700 | 453 | 4 | 412 | 3 | 31 | 2 | 0 | 1 | 0 | 0 | 0 |  | 0700 | 1 | 1 | 12 | 6 | 17 | 110 | 182 | 103 | 16 | 4 | 1 | 0 | 0 | 0 | 36.7 | 41.6 | 124 | 27.4 | 11 | 2.4 | 2 | 0.4 |
| 0800 | ${ }^{443}$ | 3 | 401 | 5 | 32 | 2 | 0 | 0 | 0 | 0 | 0 |  | 0800 | 0 | 1 | 1 | 4 | 30 | 114 | 185 | 90 | 15 | 3 | 0 | 0 | 0 | 0 | 36.7 | 41.4 | 108 | 24.4 | 13 | 2.9 | 0 |  |
| 0900 | 320 | 3 | 282 | 1 | ${ }^{31}$ | 0 | 1 | 0 | 0 | 1 | 1 |  | 0900 | 0 | 0 | 1 | 6 | 19 | 91 | 152 | 39 | 8 | 3 | 1 | 0 | 0 | 0 | 36.2 | 40 | 51 | 15.9 | 10 | 3.1 | 3 | 0.9 |
| 1000 | 307 | 1 | 268 | 2 | 35 | 0 | 0 | 0 | 1 | 0 | 0 |  | 1000 | 1 | 2 | 3 | 4 | 35 | 101 | 119 | 30 | 6 | 6 | 0 | 0 | 0 | 0 | 35 | 39.6 | 42 | 13.7 | 11 | 3.6 | 1 | 0.3 |
| 1100 | 342 | 4 | 294 | 2 | 40 | 1 | 0 | 0 | 0 | 1 | 0 |  | 1100 | 0 | 1 | 1 | 1 | 24 | 138 | 131 | 38 | 7 | 1 | 0 | 0 | 0 | 0 | 35.4 | 39.6 | 46 | 13.5 |  | 1.5 | 1 | 0.3 |
| 1200 | 329 | 3 | 293 | 1 | 27 | 1 |  | 0 | 0 | 1 | 0 |  | 1200 | 0 | 2 | 1 | 4 | 30 | 116 | 120 | 39 | 15 | 2 | 0 | 0 | 0 | 0 | 35.7 | 40.5 | 56 | 17 | 12 | 3.6 | 1 | 0.3 |
| 1300 | 329 | 6 | 273 | 5 | 42 | 1 | 1 | 0 | 1 | 0 | 0 |  | 1300 | 0 | 0 | 2 | 4 | 35 | 131 | 113 | 42 | 2 | 0 | 0 | 0 | 0 | 0 | 34.9 | 39.6 | 44 | 13.4 | 2 | 0.6 | 0 | 0 |
| 1400 | 327 | 6 | 287 | 0 | 33 | 0 | 0 | 1 | 0 | 0 | 0 |  | 1400 | 1 | 0 | 2 | 1 | 22 | 117 | 120 | 51 | 9 | 4 | 0 | 0 | 0 | 0 | 36.2 | 40.5 | 64 | 19.6 | 11 | 3.4 | 2 | 0.6 |
| 1500 | 335 | 7 | 286 | 1 | 40 | 0 | 0 | 1 | 0 | 0 | 0 |  | 1500 | 0 | 0 | 4 | 8 | 22 | 108 | 137 | 36 | 12 | 8 | 0 | 0 | 0 | 0 | 35.9 | 40.3 | 56 | 16.7 | ${ }^{16}$ | 4.8 | 1 | 0.3 |
| 1600 | 408 | 8 | 348 | 2 | 46 | 1 | 0 | 1 | 2 | 0 | 0 |  | 1600 |  | 3 | 10 | 9 | 36 | 121 | ${ }^{156}$ | 62 | ${ }^{6}$ | 5 | 0 | 0 | 0 | 0 | 35.3 | 40.7 | 73 | 17.9 | 8 |  | 1 |  |
| 1700 | 472 | 5 | 442 | 5 | 19 | 0 | 0 | 0 | 1 | 0 | 0 |  | 1700 | 0 | 1 | 1 | 5 | 29 | 161 | 155 | 92 | 24 | 3 | 1 | 0 | 0 | 0 | 36.5 | 41.6 | 120 | 25.4 | 20 | 4.2 | 1 | 0.2 |
| 1800 | 383 | 5 | 356 | 2 | 19 | 1 | 0 | 0 | 0 | 0 | 0 |  | 1800 | 0 | 5 | 3 | 11 | 38 | 106 | 134 | 63 | 16 | 7 | 0 | 0 | 0 | 0 | 35.7 | 41.8 | 86 | 22.5 | 17 | 4.4 | 3 | 0.8 |
| 1900 | 271 | 8 | 245 | 1 | 16 | 0 | 0 | 0 | 0 | 0 | 1 |  | 1900 | 0 | 0 | 0 | 0 | 5 | 78 | 117 | ${ }^{48}$ | ${ }^{13}$ | ${ }^{6}$ | 0 | 0 | 0 | 0 | 37.4 | 42.5 | 67 | 24.7 | 14 | 5.2 | 1 |  |
| 2000 | 151 | 4 | 135 | 1 | 11 | 0 | 0 | 0 | 0 | 0 | 0 |  | 2000 | 0 | 0 | 0 | 0 | 5 | 38 | 45 | 35 | 15 | 11 | 2 | 0 | 0 | 0 | 39.9 | 45.6 | 63 | 41.7 | 22 | 14.6 | 7 | 4.6 |
| 2100 | 91 | 1 | 85 | 1 | 3 | 0 | 0 | 0 | 1 | 0 | 0 |  | 2100 | 0 | 0 | 0 | 0 | 0 | 17 | 25 | 27 | 14 | 7 | 1 | 0 | 0 | 0 | 41 | 47.9 | 49 | 53.8 | 18 | 19.8 | 2 | 2.2 |
| 2200 | 75 | 1 | 69 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 |  | 2200 | 0 | 0 | 0 | 0 | 3 | 15 | 26 | 22 | 7 | 1 | 1 | 0 | 0 | 0 | 39.2 | 44.5 | 31 | 41.3 |  | 10.7 | 1 |  |
| 2300 |  |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 2300 | 0 | 0 | 0 | 0 |  | , | 12 | 7 | 4 | 4 | 3 | 1 | 0 | 0 | 43.2 | 52.3 | 19 | 50 | 10 | 26.3 | 4 | 10.5 |
| 07-19 | 4448 | 55 | 3942 | 29 | 395 | 9 | 5 | 4 | 5 | 3 | 1 |  | 07-19 | 3 | 16 | 41 | 63 | 337 | 1414 | 1704 | 685 | 136 | 46 | 3 | 0 | 0 | 0 | 35.9 | 40.7 | 870 | 19.6 | 136 | 3.1 | 16 | 0.4 |
| 06-22 | 5146 | 72 | 4557 | 32 | 453 | 10 | 7 | 4 | 6 | 3 | 2 |  | 06-22 |  | 16 | 43 | 63 | 352 | 1567 | 1955 | 856 | 202 | 83 | 6 | 0 | 0 | 0 | 36.4 | 41.4 | 1147 | 22.3 | 218 | 4.2 | 28 | 0.5 |
| 06-00 | 5259 | 74 | 4660 | 32 | 461 | 10 | 7 | 4 | 6 | 3 | 2 |  | 06-00 | 3 | 16 | 43 | 63 | 356 | 1588 | 1993 | 885 | 213 | 88 | 10 | 1 | 0 | 0 | 36.5 | 41.6 | 1197 | 22.8 | 236 | 4.5 | 33 | 0.6 |
| 00.00 | 5352 | 77 | 4739 | 32 | 471 | 11 | 7 | 4 | 6 | 3 | 2 |  | 00-00 | 3 | 16 | 43 | 64 | 360 | 1599 | 2011 | 914 | 230 | 99 | 12 | 1 | 0 | 0 | 36.6 | 41.8 | 1256 | 23.5 | 263 | 4.9 | 39 | 0.7 |

Virtual Day (1)

| Time | Total | $\underset{\substack{\text { Cls } \\ 1}}{ }$ | ${ }_{c}^{\text {cls }}$ | ${ }_{\substack{\text { cls } \\ 3}}$ | ${ }_{4}^{\mathrm{Cls}}$ | ${ }_{c}^{\text {Cls }}$ | $\underset{6}{\mathrm{Cls}} \underset{\substack{ \\\hline}}{\mathrm{~s}}$ | ${ }_{7}^{\mathrm{Cls}}$ | $\begin{gathered} \text { Cls } \\ 8 \end{gathered}$ | $\underset{9}{\mathrm{Cls}}$ | $\begin{aligned} & \text { Cls } \\ & 10 \end{aligned}$ | Fix1 | Time | $\begin{gathered} \text { Vbin } \\ 0 \\ 10 \end{gathered}$ | $\begin{aligned} & \text { Vbin } \\ & 10 \\ & 15 \end{aligned}$ | $\begin{gathered} \text { Vbin } \\ 15 \\ 20 \end{gathered}$ | $\begin{aligned} & \text { Vbin } \\ & 20 \\ & 25 \end{aligned}$ | $\begin{aligned} & \text { Vbin } \\ & 25 \\ & 30 \end{aligned}$ | $\begin{gathered} \text { Vbin } \\ 30 \\ 35 \end{gathered}$ | $\begin{gathered} \text { Vbin } \\ 35 \\ 40 \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Vbin } \\ & 40 \\ & 45 \end{aligned}$ | $\begin{gathered} \text { Vbin } \\ 45 \\ 50 \end{gathered}$ | $\begin{aligned} & \text { Vbin } \\ & 50 \\ & 60 \end{aligned}$ | $\begin{aligned} & \text { Vbin } \\ & 60 \\ & 70 \end{aligned}$ | $\begin{gathered} \text { Vbin } \\ 70 \\ 80 \end{gathered}$ | $\begin{aligned} & \text { Vbin } \\ & 80 \\ & 90 \end{aligned}$ | $\begin{gathered} \text { Vbin } \\ 90 \\ 100 \end{gathered}$ | Mean | $\underset{85}{\mathrm{v}_{\mathrm{ppp}}}$ | $\begin{aligned} & >\text { PSLL } \\ & 40 \end{aligned}$ | >PSL\% | $\begin{gathered} >\mathrm{SLL} \\ 46 \\ \text { ACPO } \end{gathered}$ | $\begin{aligned} & \text { SLIT } \mathrm{SL} \\ & 46 \\ & \text { ACPO } \end{aligned}$ | $\begin{gathered} \text { SSL2 } \\ 55 \\ \text { DFT } \end{gathered}$ | $\begin{gathered} \text { PSLL\% } \\ 55 \\ \text { DFT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0000 | 8 | 1 | 8 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0000 | 0 | 0 | 0 | 0 | 0 | 1 | ${ }_{3}^{2}$ | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 40.2 - |  | 5 | 62.5 | 0 1 | 125 | 0 |  |
| 0100 | 8 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0100 | 0 | 0 | 0 | 0 | 0 | 0 | ${ }_{0}^{3}$ | 4 | 1 | 0 | 0 | 0 | 0 | 0 | $41.5-$ 48.6 |  | 5 | 62.5 | 1 | 12.5 50 | 0 | $25$ |
| 0300 | $\stackrel{4}{4}$ | 1 | ${ }^{3}$ | 0 | 0 | 0 | 0 | 0 | ${ }_{0}^{0}$ | 0 | 0 |  | 0200 | 0 | 0 | 0 | 0 | 0 | 1 | ${ }_{2}$ | ${ }_{3}$ | 0 | 2 | 0 | 0 | 0 | 0 | ${ }_{44.7}^{48 .}{ }^{-}$ |  | 4 | 100 70 | 2 | 50 40 | 1 | 25 10 |
| 0400 | 15 | 0 | 13 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 3 | 3 | 1 | 2 | 0 | 0 | 0 | 43.7 | 57.7 | 9 | 60 | 5 | 33.3 | 3 | 20 |
| 0500 | 48 | 1 | 39 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 0 |  | 0500 | 0 | 0 | 0 | 0 | 3 | 8 | 8 | 12 | 13 | 4 | 0 | 0 | 0 | 0 | 41.5 | 49 | 29 | 60.4 | 15 | 31.3 | 1 | 2.1 |
| 0600 | 185 | 4 | 150 | 0 | 28 | 1 | 2 | 0 | 0 | 0 | 0 |  | 0600 | 0 | 0 | 2 | 0 | 1 | 20 | 64 | 61 | 24 | 13 | 0 | 0 | 0 | 0 | 40.8 | 45.6 | 98 | 53 | 28 | 15.1 | 2 | 1.1 |
| 0700 | 453 | 4 | 412 | 3 | 31 | 2 | 0 | 1 | 0 | 0 | 0 |  | 0700 | 1 | 1 | 12 | 6 | 17 | 110 | 182 | 103 | 16 |  | 1 | 0 | 0 | 0 | 36.7 | 41.6 | 124 | 27.4 | 11 | 2.4 | 2 | 0.4 |
| 0800 | ${ }^{43}$ | 3 | 401 |  | 32 | 2 | 0 | 0 | 0 | 0 | 0 |  | 0800 | 0 | 1 | 1 | 4 | 30 | 114 | 185 | 90 | 15 | 3 | 0 | 0 | 0 | 0 | 36.7 | 41.4 | 108 | 24.4 | 13 | 2.9 | 0 |  |
| 0900 | 320 | 3 | 282 | 1 | 31 | 0 | 1 | 0 | 0 | 1 | 1 |  | 0900 | 0 | 0 | 1 | 6 | 19 | 91 | 152 | 39 | 8 | 3 | 1 | 0 | 0 | 0 | 36.2 | 40 | 51 | 15.9 | 10 | 3.1 | 3 | 0.9 |
| 1000 | 307 | 1 | 268 | 2 | 35 | 0 | 0 | 0 | 1 | 0 | 0 |  | 1000 | 1 | 2 | 3 | 4 | 35 | 101 | 119 | 30 | 6 | 6 | 0 | 0 | 0 | 0 | 35 | 39.6 | 42 | 13.7 | 11 | 3.6 | 1 | 0.3 |
| 1100 | ${ }^{342}$ | 4 | 294 | 2 | 40 | 1 | 0 | 0 | 0 | 1 | 0 |  | 1100 | 0 | 1 | 1 | 1 | 24 | 138 | 131 | ${ }^{38}$ | 7 | 1 |  | 0 | 0 | 0 | 35.4 | 39.6 | 46 | 13.5 | 5 | 1.5 | 1 | 0.3 |
| 1200 | 329 | 3 | ${ }^{293}$ | 1 | 27 | 1 | 3 | 0 | 0 | 1 | 0 |  | ${ }^{1200}$ | 0 | 2 | 1 | 4 | 30 | 116 | 120 | 39 | 15 | 2 | 0 | 0 | 0 | 0 | 35.7 | 40.5 | 56 | 17 | 12 | 3.6 | 1 | 0.3 |
| 1300 | 329 | 6 | 273 | 5 | 42 | 1 | 1 | 0 | 1 | 0 | 0 |  | 1300 | 0 | 0 | 2 | 4 | 35 | 131 | 113 | 42 | 2 | 0 | 0 | 0 | 0 | 0 | 34.9 | 39.6 | 44 | 13.4 | 2 | 0.6 | 0 | 0 |
| 1400 | 327 | 6 | 287 | 0 | 33 | 0 | 0 | 1 | 0 | 0 | 0 |  | 1400 | 1 | 0 | 2 | 1 | 22 | 117 | 120 | 51 | 9 | 4 | 0 |  |  | 0 | 36.2 | 40.5 | 64 | 19.6 | 11 | 3.4 | 2 |  |
| 1500 | 335 | 7 | 286 | 1 | 40 | 0 | 0 | 1 | 0 | 0 | 0 |  | 1500 | 0 | 0 | 4 | 8 | 22 | 108 | 137 | 36 | 12 | 8 |  | 0 | 0 | 0 | 35.9 | 40.3 | 56 | 16.7 | 16 | 4.8 | 1 | 0.3 |
| 1600 | 408 | 8 | 348 | 2 | 46 | 1 | 0 | 1 | ${ }^{2}$ | 0 | 0 |  | 1600 | 0 | 3 | 10 | 9 | 36 | 121 | 156 | 62 | 6 | 5 | 0 | 0 | 0 | 0 | 35.3 | 40.7 | 73 | 17.9 | 8 | ${ }^{2}$ | 1 | 0.2 |
| 1700 | 472 | 5 | 442 | 5 | 19 | 0 | 0 | 0 | 1 | 0 | 0 |  | 1700 | 0 | 1 | 1 | 5 | 29 | 161 | 155 | 92 | 24 | 3 | 1 | 0 | 0 | 0 | 36.5 | 41.6 | 120 | 25.4 | 20 | 4.2 | 1 | 0.2 |
| 1800 | ${ }^{383}$ | 5 | ${ }^{356}$ | 2 | 19 | 1 | 0 | 0 | 0 | 0 | 0 |  | 1800 | 0 | 5 | 3 | 11 | ${ }^{38}$ | 106 | 134 | ${ }_{6}^{63}$ | ${ }^{16}$ | 7 | 0 | 0 | 0 | 0 | ${ }^{357}$ | 41.8 | ${ }^{86}$ | 22.5 | 17 | 4.4 | 3 |  |
| 1900 | 271 | 8 | 245 |  | 16 | 0 | 0 | 0 | 0 | 0 | 1 |  | 1900 | 0 | 0 | 0 | 0 | 9 | 78 | 117 | 48 | 13 | 6 | 0 | 0 | 0 | 0 | 37.4 | 42.5 | 67 | 24.7 | 14 | 5.2 | 1 |  |
| 2000 | 151 | 4 | 135 | 1 | 11 | 0 | 0 | 0 | 0 | 0 | 0 |  | 2000 | 0 | 0 | 0 | 0 | 5 | 38 | 45 | 35 | 15 | 11 |  | 0 | 0 | 0 | 39.9 | 45.6 | 63 | 41.7 | 22 | 14.6 | 7 | 4.6 |
| 2100 | 91 | 1 | 85 |  | 3 | 0 | 0 | 0 | 1 | 0 | 0 |  | 2100 | 0 | 0 | 0 | 0 | 0 | 17 | 25 | 27 | 14 | 7 |  | 0 | 0 | 0 | 41 | 47.9 | 49 | 53.8 | 18 | 19.8 | 2 | 2.2 |
| 2200 | 75 | 1 | 69 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 |  | 2200 | 0 | 0 | 0 | 0 | ${ }^{3}$ | 15 | 26 | 22 | 7 | 1 | 3 | 0 | 0 | 0 | 39.2 | 44.5 | 31 | 41.3 | 10 | 10.7 | 1 |  |
| 2300 | 38 | 1 | 34 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |  | 2300 | 0 | 0 | 0 | 0 | 1 | 6 | 12 | 7 | 4 | 4 | 3 | 1 | 0 | 0 | 43.2 | 52.3 | 19 | 50 | 10 | 26.3 | 4 | 10.5 |



Virtual Week (1)


## Grand Total



TRL LIMITED
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CAPACITIES, QUEUES, AND DELAYS AT 3 OR 4-ARM MAJOR/MINOR PRIORITY JUNCTIONS

```
PICADY 5.1 ANALYSIS PROGRAM
```

RELEASE 5.0 (JUNE 2010)
ADAPTED FROM PICADY/3 WHICH IS CROWN COPYRIGHT BY PERMISSION OF THE CONTROLLER OF HMSO

FOR SALES AND DISTRIBUTION INFORMATION,
PROGRAM ADVICE AND MAINTENANCE CONTACT:
TRL SOFTWARE SALES
TEL: CROWTHORNE (01344) 770758, FAX: 770356 EMAIL: software@trl.co.uk

THE USER OF THIS COMPUTER PROGRAM FOR THE SOLUTION OF AN ENGINEERING PROBLEM IS IN NO WAY RELIEVED OF HIS/HER RESPONSIBILITY FOR THE CORRECTNESS OF THE SOLUTION

Run with file:-
"Y:\ARDENT PROJECTS $\backslash$ F990 - Cherry Lodge Golf Club, Aperfield $\backslash$ Transport $\backslash P I C A D Y \backslash M a i n ~ R o a d ~-~ A c c e s s ~ \ ~$ F990_Main Rd_2011_PM_Ex plus dev right turn.vpi"
(drive-on-the-left) at 14:37:22 on Monday, 10 October 2011
.RUN INFORMATION

| RUN TITLE | $:$ A223 Main Road_Access_- 2011_PM |
| :--- | :--- |
| LOCATION | : Biggin Hill, Westerham |
| DATE | : 05/10/11 |
| CLIENT | : Wooodland Environmental |
| ENUMERATOR | $:$ rfisher [ARDENT45] |
| JOB NUMBER | $:$ F990 |
| STATUS | : Preliminary |
| DESCRIPTION | $:$ |
| MAJOR/MINOR JUNCTION CAPACITY AND DELAY |  |

INPUT DATA
MAJOR ROAD (ARM C) $\quad$ I

ARM A IS A233 Main Road (North)
ARM B IS Access Road
ARM C IS A233 Main Road (South)
.STREAM LABELLING CONVENTION
STREAM A-B CONTAINS TRAFFIC GOING FROM ARM A TO ARM B STREAM B-AC CONTAINS TRAFFIC GOING FROM ARM B TO ARM A AND TO ARM C ETC.
. GEOMETRIC DATA


## SLOPES AND INTERCEPT

(NB:Streams may be combined, in which case capacity will be adjusted)


| I | AM B-A | STREAM | A-C | STREAM A-B | STREAM | C-A | STREAM | C-B | I |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | 617.24 |  | 0.26 | 0.10 |  | 0.16 |  | 0.37 | I |


(NB These values do not allow for any site specific corrections)
.TRAFFIC DEMAND DATA

| I ARM I FLOW SCALE (\%) |  |  |  |
| :---: | :---: | :---: | :---: |
| I | A | I | 100 |
| I | B | I | 100 |
| I | C | I | 100 |

.Demand set: A223 Main Road_Access_ 2011_PM

TIME PERIOD BEGINS 16.00 AND ENDS 17.30
LENGTH OF TIME PERIOD - 90 MIN
LENGTH OF TIME SEGMENT - 15 MIN
.DEMAND FLOW PROFILES ARE SYNTHESISED FROM TURNING COUNT DATA

| $\begin{array}{ll}\text { I } & \text { ARM } \\ \text { I } & \\ \text { I } & \end{array}$ |  |  | I | NUMBER OF |  | MINUTES FROM START WHEN |  |  |  |  |  | I | RATE |  | OF FLOW |  | (VEH/MIN) |  | I |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | FLOW | StARTS | I | TOP | OF PEAK | I | FLO | W STOPS | I | BEFORE | I | AT | TOP | I | AFter | I |
|  |  |  | I | TO | RISE | I | IS | REACHED | I | FAL | LING | I | PEAK | I | OF | PEAK | I | PEAK | I |
|  |  |  | I |  |  | I |  |  | I |  |  | I |  | I |  |  | I |  | I |
| I | ARM | A | I |  | 15.00 | I |  | 45.00 | I |  | 75.00 | I | 5.10 | I |  | 7.65 | I | 5.10 | I |
| I | ARM | B |  |  | 15.00 | I |  | 45.00 | I |  | 75.00 | I | 0.19 | I |  | 0.28 | I | 0.19 | I |
| I | ARM | C | I |  | 15.00 | I |  | 45.00 | I |  | 75.00 | I | 6.53 | I |  | 9.79 | 1 | 6.53 | I |

. Demand set: A223 Main Road_Access_ 2011_PM


| I |  | I |  |  | I | ( 3.8) |  | ( 0.0) |  | $($ | 0.0) I |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I |  | I |  |  | I |  | I |  | I |  | I |
| I |  | I | ARM | C | I | 0.971 | I | 0.029 | I |  | 0.000 I |
| I |  | I |  |  | I | 0.0 | I | 0.0 | I |  | 0.0 I |
| I |  | I |  |  | I | ( 12.0) | I | ( 3.8) | I | $($ | 0.0) I |
| I |  | I |  |  | I |  | I |  | I |  | I |
| I | 17.00-17.15 | I |  |  | I |  | I |  | I |  | I |
| I |  | I | ARM | A | I | 0.000 | I | 0.000 | I |  | 1.000 I |
| I |  | I |  |  | I | 0.0 | I | 0.0 | I |  | 0.0 I |
| I |  | I |  |  | I | ( 0.0) | I | ( 0.0) | I | ( | 12.8) I |
| I |  | I |  |  | I |  | I |  | I |  | I |
| I |  | I | ARM | B | I | 1.000 | I | 0.000 | I |  | 0.000 I |
| I |  | I |  |  | I | 0.0 | I | 0.0 | I |  | 0.0 I |
| I |  | I |  |  | I | ( 3.8) | I | ( 0.0) | I | $($ | 0.0) I |
| I |  | I |  |  | I |  | I |  | I |  | I |
| I |  | I | ARM | C | I | 0.971 | I | 0.029 | I |  | 0.000 I |
| I |  | I |  |  | I | 0.0 | I | 0.0 | I |  | 0.0 I |
| I |  | I |  |  | I | ( 12.0) | I | ( 3.8) | I | $($ | 0.0) I |
| I |  | I |  |  | I |  | I |  | I |  | I |
| I | 17.15-17.30 | I |  |  | I |  | I |  | I |  | I |
| I |  | I | ARM | A | I | 0.000 | I | 0.000 | I |  | 1.000 I |
| I |  | I |  |  | I | 0.0 | I | 0.0 | I |  | 0.0 I |
| I |  | I |  |  | I | ( 0.0) | I | ( 0.0) | I |  | 12.8) I |
| I |  | I |  |  | I |  | I |  | I |  | I |
| I |  | I | ARM | B | I | 1.000 | I | 0.000 | I |  | 0.000 I |
| I |  | I |  |  | I | 0.0 | I | 0.0 | I |  | 0.0 I |
| I |  | I |  |  | I | ( 3.8) | I | ( 0.0) | I | ( | 0.0) I |
| I |  | I |  |  | I |  | I |  | I |  | I |
| I |  | I | ARM | C | I | 0.971 | I | 0.029 | I |  | 0.000 I |
| I |  | I |  |  | I | 0.0 | I | 0.0 | I |  | 0.0 I |
| I |  | I |  |  | I | ( 12.0) | I | ( 3.8) | I | ( | 0.0) I |
| I |  | I |  |  | I |  | I |  | I |  | I |

TURNING PROPORTIONS ARE CALCULATED FROM TURNING COUNT DATA THE PERCENTAGE OF HEAVY VEHICLES VARIES BETWEEN TIME SEGMENTS THE PERCENTAGE OF HEAVY VEHICLES VARIES OVER TURNING MOVEMENTS

|  | FOR COMBINED DEMAND SETS AND FOR TIME PERIOD |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | TIME | $\begin{array}{r} \text { DEMAND } \\ \text { (VEH/MIN) } \end{array}$ | CAPACITY <br> (VEH/MIN) | $\begin{aligned} & \text { DEMAND/ } \\ & \text { CAPACITY } \\ & (\operatorname{RFC}) \end{aligned}$ | PEDESTRIAN FLOW (PEDS/MIN) | $\begin{aligned} & \text { START } \\ & \text { QUEUE } \\ & \text { (VEHS) } \end{aligned}$ | $\begin{gathered} \text { END } \\ \text { QUEUE } \\ \text { (VEHS) } \end{gathered}$ | DELAY (VEH.MIN/ TIME SEGMENT) | GEOMETRIC DELAY <br> (VEH.MIN/ <br> TIME SEGMENT) | AVERAGE DELAY PER ARRIVING VEHICLE (MIN) |  |
| I | 16.00-16.15 |  |  |  |  |  |  |  |  |  |  |
| I | B-AC | 0.19 | 7.26 | 0.026 |  | 0.00 | 0.03 | 0.4 |  | 0.14 | I |
| I | C-AB | 0.33 | 13.24 | 0.025 |  | 0.00 | 0.03 | 0.5 |  | 0.08 | I |
| I | C-A | 6.22 |  |  |  |  |  |  |  |  | I |
| I | A-B | 0.00 |  |  |  |  |  |  |  |  | I |
| I | A-C | 5.12 |  |  |  |  |  |  |  |  | I |
| I |  |  |  |  |  |  |  |  |  |  | I |


| I | TIME | $\begin{array}{r} \text { DEMAND } \\ \text { (VEH/MIN) } \end{array}$ | CAPACITY <br> (VEH/MIN) | $\begin{aligned} & \text { DEMAND/ } \\ & \text { CAPACITY } \\ & \text { (RFC) } \end{aligned}$ | $\begin{gathered} \text { PEDESTRIAN } \\ \text { FLOW } \\ \text { (PEDS/MIN) } \end{gathered}$ | START QUEUE (VEHS) | $\begin{gathered} \text { END } \\ \text { QUEUE } \\ \text { (VEHS) } \end{gathered}$ | DELAY (VEH.MIN/ TIME SEGMENT) | GEOMETRIC DELAY (VEH.MIN/ TIME SEGMENT) | AVERAGE DELAY PER ARRIVING VEHICLE (MIN) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | 16.15-1 | . 30 |  |  |  |  |  |  |  |  |
| I | B-AC | 0.22 | 6.75 | 0.033 |  | 0.03 | 0.03 | 0.5 |  | 0.15 |
| I | $\mathrm{C}-\mathrm{AB}$ | 0.44 | 13.76 | 0.032 |  | 0.03 | 0.04 | 0.6 |  | 0.08 |
| I | C-A | 7.38 |  |  |  |  |  |  |  |  |
| I | A-B | 0.00 |  |  |  |  |  |  |  |  |
| I | A-C | 6.11 |  |  |  |  |  |  |  |  |
| I |  |  |  |  |  |  |  |  |  |  |


| I | TIME | $\begin{array}{r} \text { DEMAND } \\ \text { (VEH/MIN) } \end{array}$ | CAPACITY <br> (VEH/MIN) | $\begin{aligned} & \text { DEMAND/ } \\ & \text { CAPACITY } \\ & \text { (RFC) } \end{aligned}$ | PEDESTRIAN FLOW (PEDS/MIN) | START QUEUE (VEHS) | $\begin{gathered} \text { END } \\ \text { QUEUE } \\ \text { (VEHS) } \end{gathered}$ | $\begin{gathered} \text { DELAY } \\ \text { (VEH.MIN/ } \\ \text { TIME SEGMENT) } \end{gathered}$ | GEOMETRIC DELAY (VEH.MIN/ TIME SEGMENT) | AVERAGE DELAY PER ARRIVING VEHICLE (MIN) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | 16.30-16.45 |  |  |  |  |  |  |  |  |  |
| I | B-AC | 0.28 | 6.04 | 0.046 |  | 0.03 | 0.05 | 0.7 |  | 0.17 |
| I | $\mathrm{C}-\mathrm{AB}$ | 0.69 | 14.77 | 0.047 |  | 0.04 | 0.07 | 1.0 |  | 0.07 |
| I | C-A | 8.88 |  |  |  |  |  |  |  |  |
| I | A-B | 0.00 |  |  |  |  |  |  |  |  |
| I | A-C | 7.49 |  |  |  |  |  |  |  |  |
| I |  |  |  |  |  |  |  |  |  |  |


| I | TIME | $\begin{aligned} & \text { DEMAND } \\ & \text { (VEH/MIN) } \end{aligned}$ | CAPACITY <br> (VEH/MIN) | $\begin{gathered} \text { DEMAND/ } \\ \text { CAPACITY } \\ \text { (RFC) } \end{gathered}$ | PEDESTRIAN FLOW (PEDS/MIN) | $\begin{aligned} & \text { START } \\ & \text { QUEUE } \\ & \text { (VEHS) } \end{aligned}$ | $\begin{gathered} \text { END } \\ \text { QUEUE } \\ \text { (VEHS) } \end{gathered}$ | DELAY (VEH.MIN/ TIME SEGMENT) | GEOMETRIC DELAY (VEH.MIN/ TIME SEGMENT) | AVERAGE DELAY PER ARRIVING VEHICLE (MIN) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | 16.45-1 | . 00 |  |  |  |  |  |  |  |  |
| I | B-AC | 0.28 | 6.04 | 0.046 |  | 0.05 | 0.05 | 0.7 |  | 0.17 |
| I | C-AB | 0.69 | 14.77 | 0.047 |  | 0.07 | 0.07 | 1.1 |  | 0.07 |
| I | C-A | 8.88 |  |  |  |  |  |  |  |  |
| I | A-B | 0.00 |  |  |  |  |  |  |  |  |
| I | A-C | 7.49 |  |  |  |  |  |  |  |  |
| I |  |  |  |  |  |  |  |  |  |  |


| I | TIME | $\begin{aligned} & \text { DEMAND } \\ & \text { (VEH/MIN) } \end{aligned}$ | CAPACITY <br> (VEH/MIN) | $\begin{gathered} \text { DEMAND/ } \\ \text { CAPACITY } \\ (\operatorname{RFC}) \end{gathered}$ | PEDESTRIAN FLOW (PEDS/MIN) | $\begin{aligned} & \text { START } \\ & \text { QUEUE } \\ & \text { (VEHS) } \end{aligned}$ | $\begin{gathered} \text { END } \\ \text { QUEUE } \\ \text { (VEHS) } \end{gathered}$ | DELAY (VEH.MIN/ TIME SEGMENT) | GEOMETRIC DELAY <br> (VEH.MIN/ <br> TIME SEGMENT) | AVERAGE DELAY PER ARRIVING VEHICLE (MIN) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | 17.00-17.15 |  |  |  |  |  |  |  |  |  |
| I | B-AC | 0.22 | 6.75 | 0.033 |  | 0.05 | 0.03 | 0.5 |  | 0.15 |
| I | $\mathrm{C}-\mathrm{AB}$ | 0.44 | 13.76 | 0.032 |  | 0.07 | 0.04 | 0.7 |  | 0.08 |



| I | TIME | $\begin{array}{r} \text { DEMAND } \\ \text { (VEH/MIN) } \end{array}$ | CAPACITY <br> (VEH/MIN) | $\begin{gathered} \text { DEMAND/ } \\ \text { CAPACITY } \\ \text { (RFC) } \end{gathered}$ | $\begin{gathered} \text { PEDESTRIAN } \\ \text { FLOW } \\ \text { (PEDS/MIN) } \end{gathered}$ | START QUEUE (VEHS) | $\begin{gathered} \text { END } \\ \text { QUEUE } \\ \text { (VEHS) } \end{gathered}$ | DELAY (VEH.MIN/ TIME SEGMENT) | GEOMETRIC DELAY (VEH.MIN/ TIME SEGMENT) | AVERAGE DELAY PER ARRIVING VEHICLE (MIN) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | 17.15-17.30 |  |  |  |  |  |  |  |  |  |
| I | B-AC | 0.19 | 7.26 | 0.026 |  | 0.03 | 0.03 | 0.4 |  | 0.14 |
| I | C-AB | 0.34 | 13.24 | 0.025 |  | 0.04 | 0.03 | 0.5 |  | 0.08 |
| I | C-A | 6.21 |  |  |  |  |  |  |  |  |
| I | A-B | 0.00 |  |  |  |  |  |  |  |  |
| I | A-C | 5.12 |  |  |  |  |  |  |  |  |
| I |  |  |  |  |  |  |  |  |  |  |

*WARNING* NO MARGINAL ANALYSIS OF CAPACITIES AS MAJOR ROAD BLOCKING MAY OCCUR

| QUEUE FOR |  | B-A |
| :---: | :---: | :---: |
| TIME | NO. OF |  |
| SEGMENT | VEHICLES |  |
| ENDING |  | $\begin{gathered} \text { IN QUEUE } \\ 0.0 \end{gathered}$ |
| 16.15 |  |  |
| 16.30 |  | 0.0 |
| 16.45 | 0.0 |  |
| 17.00 | 0.0 |  |
| 17.15 | 0.0 |  |
| 17.30 | 0.0 |  |

QUEUE FOR STREAM C-AB

| -------------------------- |  |
| :--- | :---: |
| TIME | NO. OF |
| SEGMENT | VEHICLES |
| ENDING | IN QUEUE |
| 16.15 | 0.0 |
| 16.30 | 0.0 |
| 16.45 | 0.1 |
| 17.00 | 0.1 |
| 17.15 | 0.0 |
| 17.30 | 0.0 |

QUEUEING DELAY INFORMATION OVER WHOLE PERIOD

| I | STREAM | I | TOTAL DEMAND |  |  | I | * QUeUEIng * |  |  |  | I |  | INCLUSIVE QUEUEING <br> * DELAY * |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I |  | I |  |  |  | I | * DEL | A |  |  |  |  | I |
| I |  | I |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| I |  | I | (VEH) |  | VEH/H) | I | (MIN) |  |  | IN/VEH) | I |  | (MIN) |  | (MIN/VEH) | I |
| I | B-AC | I | 20.6 | I | 13.8 | I | 3.2 | I |  | 0.16 | I |  | 3.2 | I | 0.16 | I |
| I | $C-A B$ | I | 44.2 | I | 29.5 | I | 4.3 | I |  | 0.10 | I |  | 4.3 | I | 0.10 | I |
| I | C-A | I | 674.3 | I | 449.5 | I |  | I |  |  | I |  |  | I |  | I |
| I | A-B | I | 0.0 | I | 0.0 | I |  | I |  |  | I |  |  | I |  | I |
| I | A-C | I | 561.6 | I | 374.4 | I |  | I |  |  | I |  |  | I |  | I |
| I | ALL | I | 1300.7 | I | 867.1 | I | 7.6 | I |  | 0.01 | I |  | 7.6 | I | 0.01 | I |

* DELAY IS THAT OCCURRING ONLY WITHIN THE TIME PERIOD
* INCLUSIVE DELAY INCLUDES DELAY SUFFERED BY VEHICLES

WHICH ARE STILL QUEUEING AFTER THE END OF THE TIME PERIOD

* THESE WILL ONLY BE SIGNIfICANTLY DIFFERENT IF THERE IS

A LARGE QUEUE REMAINING AT THE END OF THE TIME PERIOD.
*******END OF RUN*******


[^0]:    * SSD based on Design Manual for Roads and Bridges

[^1]:    * SSD based on Design Manual for Roads and Bridges

